The Structure of Turbulence in Newtonian and Viscoelastic flows: Polymers and Drag Reduction Lectures 1/2

C.M. Casciola

carlomassimo.casciola@uniroma1.it

Dipartimento di Meccanica e Aeronautica Sapienza Università di Roma

Structures of the mechanics of complex bodies

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High Reynolds number jets



Da sinistra: Re = 5000; Re = 20000; $Re \simeq 2 \cdot 10^8$

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High Reynolds number jets





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Wall bounded flows



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Introduction

Certain polymers reduce the drag significantly wrt Newtonian

(a few ppm yield $DR = (D_0 - D_p)/D_0 \simeq 70\%$)



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Introduction

Rheological properties: viscoelasticity, shear thinning

In laminar flow a drag-reducing polymer solution (small concentration) is indistinguishable from a pure Newtonian fluid

Drag-reduction due to the polymer/turbulence interaction



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Outline

- Thu 17:00/18:00 Turbulence basics

- Fri 16:00/17:00 Turbulence & Walls

- Sat 09:00/10:00 Drag-reducing polymers

- Sat 17:00/18:00 Polymers & Turbulence



Turbulence basics

Given a body of dimension L moving with speed V through a Newtonian incompressible (isocoric) flow with viscosity μ and mass density ρ , the dissipation rate of mechanical energy per unit volume

$$\epsilon = 2\mu S$$
 : S

 $(S = 1/2(\nabla \mathbf{u} + \nabla \mathbf{u}^T)$ is the deformation rate) may be expected to scale as

$$\epsilon \propto \mu V^2 L^{-2}.$$



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In fact the correct answer at large Reynolds number $\textit{Re} = \mu\textit{VL}/\rho$ is

 $\epsilon \propto \rho V^3/L.$

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Dissipative anomaly

 $Re = 2. \times 10^4$ $Re = 5. \times 10^5$





Drag & Energy budget

$$D = \frac{1}{2} \rho V_b^2 C_D L_b^2$$
$$V_b D = \int_{\mathcal{B}} \epsilon \, dV \propto \epsilon \, L_b^3$$

$$\lim_{Re\to\infty} C_D(Re) = \tilde{C}_D$$

Dissipation independent of viscosity and set by the large scales



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The energy cascade



- Viscosity ineffective at large scales
- Energy injected at large scales moves towards small scales
- Eventually viscous dissipation is activated at small scales
- An inertial range sets in where the energy flux is constant

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Homogeneous - "isotropic" Navier Stokes turbulence

Assume the Navier Stokes equation for the solenoidal velocity field $\mathbf{u}(\mathbf{x}, t; \omega)$

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla \boldsymbol{p} + \nu \Delta \mathbf{u} + \mathbf{f}$$

in a periodic box \mathcal{D} , with initial data

$$\mathbf{u}(\mathbf{x},0)=\mathbf{u}_0(\mathbf{x})$$

subject to a large-scale Gaussian stochastic forcing $f(x, t; \omega)$

$$\langle \mathbf{f}(\mathbf{x},t)\otimes \mathbf{f}(\mathbf{x}+\mathbf{r},t+ au)
angle = C_f(\mathbf{r})\delta(au)$$

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Reynolds decomposition and turbulent kinetic energy

Define an average of q over different realizations of the process

$$\langle q(\mathbf{x},t)
angle = \lim_{N
ightarrow \mathrm{big}} rac{1}{N} \sum_{k=1}^N q(\mathbf{x},t,\omega_k)\,,$$

and its fluctuation (Reynolds decomposition)

$$q'(\mathbf{x},t,\omega) = q(\mathbf{x},t,\omega) - \langle q(\mathbf{x},t)
angle$$

The averaged kinetic energy density (energy per unit mass)

$$K(\mathbf{x}, t, \omega) = \frac{1}{2} \mathbf{u}(\mathbf{x}, t, \omega) \cdot \mathbf{u}(\mathbf{x}, t, \omega)$$

with Reynolds decomposition is

$$\langle \mathcal{K}(\mathbf{x},t) \rangle = \frac{1}{2} \langle \mathbf{u}(\mathbf{x},t) \cdot \langle \mathbf{u}(\mathbf{x},t) \rangle + \frac{1}{2} \langle \mathbf{u}'(\mathbf{x},t) \cdot \langle \mathbf{u}'(\mathbf{x},t) \rangle = \\ \mathcal{K}_{\mathcal{M}}(\mathbf{x},t) + \mathcal{K}_{\mathcal{T}}(\mathbf{x},t)$$

The equation for mean field and fluctuations

Averaging NS yields the equation for the mean field $\langle \mathbf{u} \rangle$:

$$\frac{\partial \langle \mathbf{u} \rangle}{\partial t} + \langle \mathbf{u} \rangle \cdot \nabla \langle \mathbf{u} \rangle = -\nabla \langle \boldsymbol{p} \rangle + \nu \Delta \langle \mathbf{u} \rangle + \langle \mathbf{f} \rangle - \nabla \cdot \langle \mathbf{u}' \otimes \mathbf{u}' \rangle$$

- Equation not closed: Reynolds stresses $\boldsymbol{\Sigma}_R = -\langle \boldsymbol{\mathsf{u}}' \otimes \boldsymbol{\mathsf{u}}'
angle.$

The equation for the fluctuation is then

$$\begin{aligned} \frac{\partial \mathbf{u}'}{\partial t} + \langle \mathbf{u} \rangle \cdot \nabla \mathbf{u}' &= -\nabla p' + \nu \Delta \mathbf{u}' + \mathbf{f}' \\ -\nabla \cdot \left[\mathbf{u}' \otimes \mathbf{u}' - \langle \mathbf{u}' \otimes \mathbf{u}' \rangle + \langle \mathbf{u} \rangle \otimes \mathbf{u}' \right] \end{aligned}$$

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The equation for the TKE

The turbulent kinetic energy $K_T(\mathbf{x}, t) = 1/2 \langle \mathbf{u}' \cdot \mathbf{u}' \rangle$ obeys an evolution equation derived from NS

$$\frac{\partial K_{T}}{\partial t} + \nabla \cdot \left(\langle \mathbf{u} \rangle K_{T} \right) = \nabla \cdot \boldsymbol{\phi}_{T} + \pi_{\tau} - \epsilon_{\tau} + \langle \mathbf{f}' \cdot \mathbf{u}' \rangle$$

-
$$\phi_T = -\langle p' \mathbf{u}' + 1/2 {u'}^2 \mathbf{u}' - \mathbf{u}' \cdot \mathbf{\Sigma}' \rangle$$
 is the spatial flux of TKE
($\mathbf{\Sigma}' = \nu (\nabla \mathbf{u}' + \nabla \mathbf{u}'^T)$)

- π_τ = ⟨**u**' ⊗ **u**'⟩: ∇⟨**u**⟩ is the production rate of TKE (conservative exchange from mean flow to fluctuations)
- $\epsilon_{\tau} = \langle \mathbf{\Sigma}' : (\nabla \mathbf{u}' + \nabla \mathbf{u}'^{T}) / 2 \rangle$ is the dissipation rate of TKE (semi-positive definite and zero only for rigid fluctuations)

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The equation for the TKE (homogeneous-isotropic)

The turbulent kinetic energy $K_T(\mathbf{x}, t) = 1/2 \langle \mathbf{u}' \cdot \mathbf{u}' \rangle$ obeys an evolution equation derived from NS

$$\frac{\partial K_{T}}{\partial t} = -\epsilon_{\tau} + \langle \mathbf{f}' \cdot \mathbf{u}' \rangle$$

- $\langle \boldsymbol{u} \rangle = 0$ by suitable choice of reference frame

- $\epsilon_{\tau} = \langle \mathbf{\Sigma}' : (\nabla \mathbf{u}' + \nabla \mathbf{u}'^{T}) / 2 \rangle$ is the dissipation rate of TKE (semi-positive definite and zero only for rigid fluctuations)

 Statistically stationary forcing and dissipation anomaly => the power extracted from the forcing is viscosity independent (provided the Reynolds number is large enough!)

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Warning on dissipation anomaly

- It is hard to predict the existence of cat's whisker from Schroedinger equation ...

Once you observe a cat however ... the whisker tells you something about the equation ...

Similarly, dissipation anomaly is a phenomenology suggested by experimental observation. It is used as an additional axiom to learn more about turbulence.

- It should be taken by no means to imply the power extracted from the external source if determined by dissipation.
- It means instead: The large scales which couple to the forcing are viscosity-independent.

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Implication of dissipation anomaly

- $\epsilon_{\tau}=2\nu \langle {\bf S}':{\bf S}'\rangle$ independent of ν implies

$$|
abla {f u}'| \propto rac{1}{\sqrt{
u}}$$

i.e. the field becomes singular as the viscosity is reduced (the Reynolds number increases).

- Since $\nabla \cdot \mathbf{u}' = 0$, $|\nabla \mathbf{u}'| \propto |\omega'|$, with $\omega' = \nabla \times \mathbf{u}'$ the vorticity fluctuation, one has

$$|oldsymbol{\omega}| \propto rac{1}{\sqrt{\iota}}$$

(in h.i.t. $\epsilon_\tau=2\nu\langle\omega'\cdot\omega'\rangle$, with $\Omega_\tau=1/2\langle\omega'\cdot\omega'\rangle$ the turbulent enstrophy.)

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Vorticity transport equation and enstrophy

- By taking the curl of NS one ends up with the transport equation for the fluctuating vorticty $\partial \omega' / \partial t + \langle \mathbf{u} \rangle \cdot \nabla \omega' = \dots$
- The equation for the turbulent enstrophy is then

$$\begin{aligned} \frac{\partial \Omega_{\tau}}{\partial t} + \mathbf{u} \cdot \nabla \Omega_{\tau} + \nabla \cdot \langle \frac{{\omega'}^2}{2} \mathbf{u}' \rangle + \langle \boldsymbol{\omega}' \otimes \mathbf{u}' \rangle : \nabla \langle \boldsymbol{\omega} \rangle = \\ \langle \boldsymbol{\omega}' \otimes \langle \boldsymbol{\omega} \rangle : \nabla \mathbf{u}' \rangle + \langle \boldsymbol{\omega}' \otimes \boldsymbol{\omega}' : \nabla \mathbf{u}' \rangle + \langle \boldsymbol{\omega}' \otimes \boldsymbol{\omega}' \rangle : \nabla \langle \mathbf{u} \rangle \\ + \nu \Delta \Omega_{\tau} - \nu \langle \nabla \boldsymbol{\omega}' : \nabla \boldsymbol{\omega}' \rangle + \langle \boldsymbol{\omega}' \cdot \nabla \times \mathbf{f}' \rangle \end{aligned}$$

- In h.i.t. ($\langle {\bf u} \rangle = \langle {\boldsymbol \omega} \rangle = 0)$ it reduces to

$$\frac{\partial \Omega_{\tau}}{\partial t} = \langle \boldsymbol{\omega}' \otimes \boldsymbol{\omega}' : \nabla \mathbf{u}' \rangle - \nu \langle \nabla \boldsymbol{\omega}' : \nabla \boldsymbol{\omega}' \rangle$$

(where the fluctuating force is conservative, $\nabla \times \mathbf{f}' = 0$).

- In stat. steady h.i.t. enstrophy production is positive, $\langle \boldsymbol{\omega}' \otimes \boldsymbol{\omega}' : \nabla \mathbf{u}' \rangle = \nu \langle \nabla \boldsymbol{\omega}' : \nabla \boldsymbol{\omega}' \rangle > 0.$

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Correlation tensor

One defines a (single-time) correlation tensor

$$\mathbf{C}(\mathbf{x},\mathbf{r},t) = \langle \mathbf{u}'(\mathbf{x}+\mathbf{r},t) \otimes \mathbf{u}'(\mathbf{x},t) \rangle \qquad \qquad C_{\alpha\beta} = \langle u'_{\alpha}(\mathbf{x}+\mathbf{r},t) u'_{\beta}(\mathbf{x},t) \rangle$$

typically with finite correlation length L_0 ,

$$\mathbf{C}(\mathbf{x},\mathbf{r},t)\simeq 0 \qquad \qquad |\mathbf{r}|>L_0 \; .$$

As a consequence, extensive quantities *do not fluctuate* in the limit of a large domain

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Example: Fluctuation intensity in the tke

Define the turbulent kinetic energy of a certain realization $\mathbf{u}(\mathbf{x}, t, \omega)$

$$\mathrm{K}_{\mathcal{T}}(t,\omega) = \int_{\mathcal{D}} \mathcal{K}_{\mathcal{T}}(\mathbf{x},t,\omega) dV_{\mathbf{x}} \; .$$

Its fluctuation is

$$\mathrm{K}_{\mathcal{T}}'(t,\omega) = \mathrm{K}_{\mathcal{T}}(t,\omega) - \langle \mathrm{K}_{\mathcal{T}}(t) \rangle$$

and we have

$$\langle \mathbf{K}_{T}'(t)^{2} \rangle = \sum_{rs} \int_{\mathcal{D}_{r}} \int_{\mathcal{D}_{s}} \langle \mathcal{K}_{T}'(\mathbf{x}, t, \omega) \mathcal{K}_{T}'(\mathbf{y}, t, \omega) \rangle dV_{x} dV_{y}$$

$$\simeq n \langle \left[\int_{\mathcal{D}_{1}} \mathcal{K}_{T}'(\mathbf{x}, t) dV_{x} \right]^{2} \rangle; \qquad \frac{\sqrt{\langle \mathbf{K}_{T}'(t)^{2} \rangle}}{\langle \mathcal{K}_{T}(t) \rangle} \simeq 1/\sqrt{n}$$

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Example: Drag force exerted on a body

Define the drag force of a certain realization $\mathbf{u}(\mathbf{x}, t, \omega)$

$$\mathrm{D}(t,\omega) = \hat{\mathbf{U}}_{\infty} \cdot \int_{\partial \mathcal{B}} \mathbf{T}(\mathbf{x},t,\omega) \cdot \mathbf{n}(\mathbf{x}) dS_{\mathbf{x}} \; .$$

Its fluctuation is

$$\mathrm{D}'(t,\omega) = \mathrm{D}(t,\omega) - \langle \mathrm{D}(t) \rangle$$

and we have

$$\sqrt{\langle {
m D}'(t)^2
angle}\simeq rac{1}{\sqrt{n}}\langle D(t)
angle$$

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Kármán-Howarth equation

Homogeneous, isotropic, stationary turbulence

- 1. Take the Navier Stokes equations for $\mathbf{u}_1' = \mathbf{u}'(\mathbf{x}_1)$ at \mathbf{x}_1
- 2. Scalar multiply by $\mathbf{u}_2' = \mathbf{u}'(\mathbf{x}_2)$, $\mathbf{x}_2 = \mathbf{x}_1 + \mathbf{r}$
- 3. Repeat steps 1-2 by exchanging points \mathbf{x}_1 and \mathbf{x}_2
- Add the two equations up Let's introduce the change of variables (x₁, x₂) → (x_c, r), with x_c = 1/2 (x₁ + x₂), r = x₂ - x₁. Two-point averages depend only on separation r (∇_c = 0),

$$abla_{2/1} = \pm
abla_r \qquad \qquad \frac{\partial}{\partial x_{2/1}^{lpha}} = \pm \frac{\partial}{\partial r^{lpha}}$$

Terms involving pressure vanish by "integration by parts" $\langle \mathbf{u}_2 \cdot \nabla_1 p'_1 \rangle = \nabla_1 \cdot \langle \mathbf{u}_2 p'_1 \rangle = -\nabla_r \cdot \langle \mathbf{u}_2 p'_1 \rangle = -p'_1 \nabla_2 \cdot \mathbf{u}'_2 = 0$

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$$abla_{2/1} = \pm
abla_r \qquad \qquad \frac{\partial}{\partial x_{2/1}^{lpha}} = \pm \frac{\partial}{\partial r^{lpha}}$$

Terms arising from the convective part take the form $\langle \mathbf{u}_2' \cdot \nabla_1 \cdot \mathbf{u}_1' \otimes \mathbf{u}_1' \rangle = \nabla_1 \cdot \langle \mathbf{u}_1' \cdot \mathbf{u}_2' \mathbf{u}_1' \rangle = -\nabla_r \cdot \langle \mathbf{u}_1' \cdot \mathbf{u}_2' \mathbf{u}_1' \rangle$

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- 3. Repeat steps 1-2 by exchanging points \mathbf{x}_1 and \mathbf{x}_2
- 4. Add the two equations up

On account of homogeneity and solenoidality one gets the Kármán-Howarth (KH) equation $(\delta u' = u'_2 - u'_1)$

$$\frac{\partial \langle \mathbf{u}_{1}' \cdot \mathbf{u}_{2}' \rangle}{\partial t} + \nabla_{r} \cdot \langle \left(\mathbf{u}_{1}' \cdot \mathbf{u}_{2}' \right) \, \delta \mathbf{u}' \rangle = \langle \mathbf{f}_{1}' \cdot \mathbf{u}_{2}' + \mathbf{f}_{2}' \cdot \mathbf{u}_{1}' \rangle + 2\nu \Delta_{r} \langle \mathbf{u}_{1}' \cdot \mathbf{u}_{2}' \rangle$$

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The energy spectrum

The trace of the correlation tensor $C(\mathbf{r}) = \operatorname{tr} [\mathbf{C}(\mathbf{r})] = \langle \mathbf{u}_1' \cdot \mathbf{u}_2' \rangle$ is the object appearing in the Kármán-Howarth equation.

- Its Fourier transform defines the energy spectrum

$$E(\mathbf{k},t) = \frac{1}{(2\pi)^3} \int_{\mathbf{R}^3} C(\mathbf{r}) e^{-j\mathbf{k}\cdot\mathbf{r}} dV_r = \mathcal{F}[C]$$

Then

$$\mathcal{K}_{T}(t) = rac{1}{2} \int E(\mathbf{k}, t) dV_{k}$$
 $\epsilon_{\tau} = rac{1}{2} \nu \int k^{2} E(\mathbf{k}, t) dV_{k}$

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The energy flux in wave-number space

The energy flux in the sapce of scales is defined as

$$abla_k \cdot \boldsymbol{\phi}_k = \jmath \mathbf{k} \cdot \mathbf{T}(\mathbf{k}, t)$$

with

$$\mathbf{T}(\mathbf{k},t) = rac{1}{(2\pi)^3} \int \langle \mathbf{u}_1' \cdot \mathbf{u}_2' \delta \mathbf{u}'
angle e^{-\jmath \mathbf{k} \cdot \mathbf{r}} dV_r$$

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The spectral view

The Fourier transform of the Kármán -Howarth equation is then

$$\frac{\partial E(\mathbf{k},t)}{\partial t} - \nabla_k \cdot \phi_k(\mathbf{k},t) = -\nu k^2 E(\mathbf{k},t) + F(\mathbf{k},t)$$
$$(F = \mathcal{F}[\langle \mathbf{u}_1' \cdot \mathbf{f}_2' + \mathbf{u}_2' \cdot \mathbf{f}_1' \rangle]).$$

Since $\phi_k(\mathbf{k}) = \phi(k) \hat{\mathbf{k}} \ (\hat{\mathbf{k}} = \mathbf{k}/k)$, with the spherical averages

$$ar{E}(k) = rac{1}{4\pi} \int_{\Omega} k^2 E(\mathbf{k}) d\Omega \qquad \quad ar{\Phi}_k(k) = rac{1}{4\pi} \int_{\Omega} k^2 \phi_k(\mathbf{k}) d\Omega \,,$$

the equation for the spectrum reads

$$rac{\partial ar{E}(k,t)}{\partial t} = rac{\partial ar{\Phi}_k(k,t)}{\partial k} - 2
u k^2 ar{E}(k,t) + ar{F}(k,t)$$

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Spectral balance in the low-wn (forcing) range $k \leq k_F$

Assume $\overline{F}(k, t)$ of compact support in k-space, i.e. $\overline{F}(k, t) \equiv 0$ for $k > k_F$. In the low wave-number band $0 \le k \le k_F$ integrate to get

$$\frac{d}{dt}\int_0^{k_F} \bar{E}(k,t) = \bar{\Phi}_k(k_F,t) - 2\nu \int_0^{k_F} k^2 \bar{E}(k,t) dk + \int_0^{k_F} \bar{F}(k,t) dk$$

In a statistically steady state, decreasing ν one ends up with

$$\bar{\Phi}_k(k_F) = -\int_0^{k_F} \bar{F}(k) dk$$

We have an energy flux across k_F from low to high wavenumbers $\bar{\Phi}_k(k_F)$ which exactly removes the power injected by the forcing

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Spectral balance in the high-wn (dissipative) range $k_F \ll k_D \leq k$

Now $\nu k^2 \overline{E}(k, t) \equiv 0$ for $k < K_D(\nu)$. In the high wave-number band $k_D(\nu) \le k < +\infty$ integrate to get

$$rac{d}{dt}\int_{k_D}^{+\infty}ar{E}(k,t)=-ar{\Phi}_k(k_D,t)-2
u\int_{k_D}^{+\infty}k^2ar{E}(k,t)dk$$

In a statistically steady state, one ends up with

$$ar{\Phi}_k(k_D) = -2
u \int_{k_D}^{+\infty} k^2 ar{E}(k,t) dk$$

We have an energy flux across k_D entering the high wn-band which feeds the scales where energy dissipation takes place

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Spectral balance in the intermediate (inertial) range $k_F \ll k \ll k_D$

Now $\nu k^2 \overline{E}(k, t) = \overline{F}(k, t) \equiv 0$ for $k_F \ll K \ll K_D(\nu)$. In the inertial band $k_F \ll K \ll K_D(\nu)$ integrate to get

$$rac{d}{dt}\int_{k_1}^{k_2}ar{E}(k,t)=ar{\Phi}_k(k_2,t)-ar{\Phi}_k(k_1,t)$$

In a statistically steady state, one ends up with

$$\bar{\Phi}_k(k_2) = \bar{\Phi}_k(k_1) = \bar{\Phi}_k(k_F) = \bar{\Phi}_k(k_D)$$

Constant energy flux across the inertial range $\bar{\Phi}_k(k) = \bar{\Phi}_0$.

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Energy transfer through the inertial range

The energy balance, $\epsilon_{\tau} = \langle \mathbf{u}' \cdot \mathbf{f}' \rangle$, leads to the conclusion that

$$\bar{\Phi}_0 \equiv 2\epsilon_\tau = 2 \langle \mathbf{u}' \cdot \mathbf{f}' \rangle$$

Dimensional analisys provides an estimate for the viscous scale,

$$\eta = \left(\frac{\nu^3}{\epsilon_{\tau}}\right)^{1/4}$$

$$\bar{E}(k) = h(k, \nu, \epsilon_{\tau}; k_F) \qquad => \qquad \frac{\bar{E}}{\epsilon_{\tau} k^{-5/3}} = h^*(k\eta, \frac{k_F}{k})$$

- When $k>>k_F$, $E/(\epsilon_ au k^{-5/3})\simeq h^*(k\eta,0)=h_0^*(k\eta)$
- In the inertial range, $k\eta << 1$, $h_0^*(k\eta) \simeq h_0^*(0) = \mathcal{C}_{\mathcal{K}}$

$$ar{E}(k)\simeq C_k\epsilon_{ au}k^{-5/3}$$

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From KH to Kolmogorov

Homogeneous, isotropic, stationary turbulence

- 1. Define $\delta \mathbf{u} = \mathbf{u}_2 \mathbf{u}_1$, $\delta u^2 = \delta \mathbf{u} \cdot \delta \mathbf{u}$
- 2. In the KH equation express (homogeneity)

$$\begin{array}{l} - \nabla_r \cdot \langle \mathbf{u}_1 \cdot \mathbf{u}_2 \delta \mathbf{u} \rangle = 1/2 \nabla_r \cdot \langle \delta u^2 \delta \mathbf{u} \rangle \\ - \langle \mathbf{u}_1 \cdot \mathbf{u}_2 \rangle = -1/2 \langle \delta u^2 \rangle + \langle u^2 \rangle \\ - \langle \mathbf{f}_2 \cdot \mathbf{u}_1 + \mathbf{f}_1 \cdot \mathbf{u}_2 \rangle = -\langle \delta \mathbf{f} \cdot \delta \mathbf{u} \rangle + 2 \langle \mathbf{f} \cdot \mathbf{u} \rangle \end{array}$$

3. Use the turbulent kinetic energy equation $\langle {\bf f} \cdot {\bf u} \rangle = \epsilon_\tau$

It follows a form of the Kolmogorov equation (see e.g. Frish)

$$\frac{\partial \langle \delta u^2 \rangle}{\partial t} + \nabla_r \cdot \underbrace{\langle \delta u^2 \delta \mathbf{u} \rangle}_{=} -4 \langle \epsilon_\tau \rangle + 2 \langle \delta \mathbf{f} \cdot \delta \mathbf{u} \rangle + 2\nu \Delta_r \langle \delta u^2 \rangle$$

Flusso Φ_r nello spazio delle scale

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Kolmogorov equation

In isotropic conditions ($\hat{\mathbf{r}} = \mathbf{r}/r$)

$$\mathbf{\Phi}_r = \Phi_r \hat{\mathbf{r}}, \qquad \Phi_r = \delta u^2 \delta u_r$$

$$abla_r \cdot \mathbf{\Phi} = rac{1}{r^2} rac{d}{dr} \left(r^2 \Phi_r
ight) \qquad \qquad rac{1}{r^2} rac{d}{dr} \left(r^2 \Phi_r
ight) \simeq -4 \langle \epsilon
angle$$

$$\Phi_r = -\frac{4}{3} \langle \epsilon \rangle r + \text{corrections} + \text{unsteadiness}$$

- Small scale corrections due to diffusion by viscosity
- Large scale corrections due to velocity-forcing correlation
- Under isotropy we also have $\langle \delta u^2 \delta u_r \rangle = 5/3 \langle \delta u_r^3 \rangle \ (\delta u_r \equiv \delta u_L)$

One finally has

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Consequences of Kolmogorov equation

- In the inertial range $r >> \eta$

$$\langle \delta u_L^3 \rangle = -\frac{4}{5} \epsilon_\tau r$$

- In the dissipative range $r\simeq\eta$

$$\nu \frac{d\langle \delta u_L^2 \rangle}{dr} = \frac{2}{15} \epsilon_\tau r \qquad = > \qquad \langle \delta u_L^2 \rangle = \frac{1}{15\nu} \epsilon_\tau r^2$$

- In the inertial range $\delta u_L \propto \epsilon_{ au}^{1/3} r^{1/3}$
- In the dissipative range $\delta u_L \propto \epsilon_{ au}^{1/2} r$
- Order of magnitude estimate for the gradients

$$|
abla {f u}'| \propto \sqrt{rac{\epsilon_ au}{15
u}} = \mathcal{O}(1/\sqrt{
u})$$

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Kolmogorov '41 Theory

For isotropic ensembles the pdf of velocity increments

$$\delta u(r) = [\mathbf{u}(\mathbf{x} + \mathbf{r}) - \mathbf{u}(\mathbf{x})] \cdot \frac{\mathbf{r}}{r}$$

is invariant under rotations For its characteristic function

$$\hat{p}(s,r) = \frac{1}{2\pi} \int p(\delta u, r) e^{-\jmath s \, \delta u} d(\delta u)$$

we have

$$\hat{p}(s,r) = \sum_{k} \frac{(-\jmath s)^{k}}{k!} \langle (\delta u)^{k} \rangle$$



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K'41 Theory

The structure functions depend on ϵ and ν and dimensional analysis yields

$$\langle [\delta u(r)]^k \rangle = S_k(r; \epsilon, \nu) = C_k f_k(r/\eta) (\epsilon r)^{k/3}$$

where the Kolmogorov scale is

$$\eta = \left(\frac{\rho\nu^3}{\epsilon}\right)^{1/4}$$

In the Inertial Range $(r/\eta
ightarrow \infty, \ f_k
ightarrow 1)$

$$S_k(r) \propto \epsilon^{k/3} r^{k/3}$$

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Intermittency

In fact dissipation is a highly intermittent field $\epsilon = \epsilon(\mathbf{x}, t)$. In a ball \mathcal{B}_r of radius r the spatial average dissipation

$$\epsilon_r = rac{3}{4\pi r^3} \int_{\mathcal{B}_r} \epsilon(\mathbf{x},t) d^3 \mathbf{x}$$

is itself a stochastic variable, and its moments manifest scaling laws of the form

$$\langle (\epsilon_r)^k
angle \propto r^{ au(k)}$$

The flatness

$$F_4(r) = rac{\langle (\epsilon_r)^4
angle}{\langle (\epsilon_r)^2
angle^2}$$

increases decreasing the scale in the inertial range $(\lim_{r\to 0} \lim_{Re\to\infty} F_4(r, Re) = \infty).$

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Intermittency corrections and K'62

The intermittency of the dissipation field affects the structure functions

$$\langle (\delta u)^k \rangle \propto \langle (\epsilon_r)^{k/3} \rangle r^{k/3} \propto r^{\zeta(k)}$$

where the scaling exponents include intermittency corrections

$$\zeta(k) = k/3 + \tau(k/3)$$





Multifractal formalism



In a stat. homogeneous Hölder continous field $|\mathbf{u}(y) - \mathbf{u}(x)| \leq \phi |\mathbf{y} - \mathbf{x}|^{h(\mathbf{x})} \text{ the pdf } p(h) \text{ is } \mathbf{x}\text{-independent.}$ The exponent h is found on a set $\mathcal{S}(h)$ of dimension D(h). The probability a ball \mathcal{B}_r intersects $\mathcal{S}(h)$ is $P \propto r^{3-D(h)}$ The scaling $\delta u^k \propto r^{kh_0}$, $h_0 \in [h, h + dh]$, occurs with probability $p(h)r^{3-D(h)}dh$

$$\langle (\delta u)^k \rangle \propto \int p(h) r^{kh+3-D(h)} dh$$

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Multifractal formalism II





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